

High-Performance High-Power Inductor Design for High-Frequency Applications

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High-Power Inductors



Air-core inductors dominate this application space due to the design challenges posed by copper and core losses in cored magnetics at HF

Air-core Inductors

Simple and easy to fabricate

Uncontrolled and unshielded fields lead to

- Electromagnetic Interference (EMI)
- Eddy current losses

Requires placement in a metal enclosure isolated from

other circuit component

Bottleneck for system miniaturization and efficiency



HF Cored Inductors



Need HF cored inductors that are efficient and provide self-shielding

500 nH 80 A_{nk} @ 13.56 MHz

Goal : Achieve high Q while ensuring minimal external magnetic field

Design guidelines

Modified pot core structure with an outer shield

Low-loss design techniques

Mitigating and modeling 3D effects

- Experimental verification
- Performance comparison to an air-core inductor

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Low-loss design techniques

- 1. Field shaping
- 2. Quasi-distributed gaps

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Current crowds due to imbalanced fields (single-sided conduction)

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Image : C. Sullivan, PSMA, 2016, High frequency magnetics design overview and winding loss [PPT Slides] J. Hu and C. Sullivan, "The quasi-distributed gap technique for planar inductors: design guidelines," IAS, 1997

Quasi-distributed

Goal : Achieve high Q while ensuring minimal external magnetic field

Low-turn count \rightarrow 3D effects 80/ Phi-directed fields Core loss in outer shell B-field in Z-directed outer shell current Additional inductance Outer shell notches

Increases reluctance of phi-directed path

Outer shell notch

Goal : Achieve high Q while ensuring minimal external magnetic field

Low-turn count \rightarrow 3D effects

Phi-directed fields

- Core loss in outer shell
- Additional inductance

Outer shell notches

Increases reluctance of phi-directed path

Reduces **core loss** in outer shell



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Low-turn count \rightarrow 3D effects

Phi-directed fields

- Core loss in outer shell
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Self-Shielded Inductor Prototype

Optimized for total loss for the given

design constraints

Design Constraints

| Inductance | 570 nH |
|--------------|--------------|
| Frequency | 13.56 MHz |
| Peak Current | 80 A |
| Power Rating | 155 kVA |
| Volume | 1.6 L |
| Material | Fair-Rite 67 |

103.8 mm



Q - Measurement Setup



Matching Network and transformer coupled resonant tank

Results



• Q- Measurement

Results





Self-Shielding Test Setup

High Q (1050, <10 % degradation) near a large metallic object (~25 mm)

Air-core Comparison

| - | | | |
|------------------------------|-------------------|------------------------|--|
| | Air-core Inductor | Self-Shielded Inductor | |
| Inductance | 585 nH | 570 nH | |
| Large – signal Q measurement | 750 | 1150 | |

Air-core Comparison

| | | 5.25x Q 3.5x lower volume |
|------------------------------|-------------------|---------------------------------|
| | Air-core Inductor | Self-Shielded Inductor |
| Inductance | 585 nH | 570 nH |
| Large – signal Q measurement | 750 | 1150 |
| Shielding Q measurement | 200 | 1050 |
| Volume | 5.57 L | 1.6 L |

Self-Shielded inductor provides improved combination of

efficiency and size

Achieves a high Q while ensuring minimal external magnetic field

Modified pot core structure with an outer shield

| Low-loss design techniques | Inductance | 570 nH | | ר |
|------------------------------------|----------------|----------------------------|---------------|--------|
| Field shaping | Frequency | 13.56 MHz | CONTRACTOR OF | |
| Quasi-distributed gaps | Peak Current | 80 A | A | 192 mm |
| | Power Rating | 155 kVA | | |
| Mitigating and modeling 3D effects | Quality factor | 1050 (5.25x higher) | | |
| Phi –directed fields | Volume | 1.6 L (3.5x lower) | |] |
| End-turns effect | | | | |

Prototype

Enable improved efficiency and miniaturization of high-power HF applications

103.8 mm

References

- R. S. Bayliss, R. S. Yang, A. J. Hanson, C. R. Sullivan, and D. J. Perreault, "Design, implementation, and evaluation of high-efficiency high-power radio-frequency inductors," in APEC, 2021
- 2. R. S. Yang, A. J. Hanson, B. A. Reese, C. R. Sullivan, and D. J. Perreault, "A low-loss inductor structure and design guidelines for high-frequency applications," IEEE Transactions on Power Electronics, 2019
- 3. R. S. Yang, A. J. Hanson, C. R. Sullivan, and D. J. Perreault, "Design flexibility of a modular lowloss high-frequency inductor structure," IEEE Transactions on Power Electronics, 2021
- 4. J. Hu and C. Sullivan, "The quasi-distributed gap technique for planar inductors: design guidelines," in IAS , 1997